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**ANTIMICROBIAL, BEVERAGE COMPATIBLE
CONVEYOR LUBRICANT**

BACKGROUND OF THE INVENTION

1. Field of the Invention

10 The present invention relates to lubricants, especially antimicrobial lubricants, and most especially to antimicrobial lubricants for use in conveyor systems for beverage containers. The lubricants are compatible with beverages and may display reduced deposition of solid materials after the lubricants have contacted spilled beverage.

2. Background of the Art

15 In the commercial distribution of most beverages, the beverages are packaged in containers of varying sizes, such containers being in the form of cartons, cans, bottles, tetrapack packages, waxed carton packs, and other forms of
20 containers. In most packaging operations, the containers are moved along conveying systems, usually in an upright position (with the opening of the container facing vertically up or down), and moved from station to station, where various operations are performed (e.g., filling, capping, labeling, sealing, etc.). The containers, in addition to their many possible formats and constructions, may
25 comprise many different types of materials, such as metals, glasses, ceramics, papers, treated papers, waxed papers, composites, layered structures, and polymeric materials (e.g., especially polyolefins such as polyethylene, polypropylene, polystyrene and blends thereof, polyesters such as polyethyleneterephthalate and polyethylenenaphthalate and blends thereof, polyamides, polycarbonates, etc.).

There are a number of different requirements which are essential or desirable for antimicrobial lubricants in the conveying systems used to carry containers for beverages. The essential requirements are that the material provide an acceptable level of lubricity for the system and that the lubricant displays an acceptable antimicrobial activity. It is also desirable that the lubricant have a viscosity which allows it to be applied by conventional pumping and/or application apparatus (e.g., spraying, roller coating, wet bed coating, etc.) as commonly used in the beverage conveyor lubricating art, and that the lubricant is beverage compatible so that it does not form solid deposits when it accidentally contacts spilled beverage on the conveyor system. This last requirement can be especially important since the formation of deposits on the conveyor will change the lubricity of the system and could require shut-down of the equipment to facilitate cleaning. Deposits may occur from the combination of beverage and lubricant in a number of different chemical methods, depending upon the particular beverage and lubricant used. One of the more common forms of deposit is caused by the formation of micelles from the interaction of species, especially different ionic species within the two materials.

Different types of lubricants have been used in the beverage conveying industry with varying degrees of success. A more common type of lubricant is the fatty acid lubricant (either the acid itself or amine salt and/or ester derivatives thereof), some of which are described in U.S. Patent No. 5,391,308. Another type of lubricant used within this field is the organic phosphate ester, as shown in U.S. Patent No. 4,521,321 and PCT Application WO 96/02616, based upon British Patent Application 94/14442.5 filed 18 July 1994 (PCT/GB95/01641).

U.S. Patent No. 5,391,308 discloses phosphate esters other than alkyl or linear esters (e.g., the alkyl aryl phosphate esters described on column 6, lines 11-20 used in combination with the alkyl or linear phosphate esters). The lubricant system

of this patent also requires the use of an aqueous based long chain fatty acid composition at a pH of from 9.0 to 10.5 as the lubricant, with specifically combined ingredients to avoid stress cracking in polyethylene terephthalate (PET) bottles transported on a conveyor system. The aromatic-polyoxyalkyl esters are
5 specifically disclosed as part of a combination of esters (along with the alkyl esters) which

“...results in substantial reduction in stress cracking, thus functioning as the stress cracking inhibiting agent, as well as the emulsifying agent, in the aqueous lubricant concentrate.@ (Column 3, lines 48-52). “

10 The reference is specific to fatty acid lubricants, and the specification points out that the use of potassium hydroxide as the saponifying agent, in fatty acid lubricants, has been found to contribute to and to promote stress cracking in P.E.T. (polyethylene terephthalate) bottles. A blend of alkyl phosphate esters and aromatic phosphate esters are shown in combination with the fatty acid lubricant to reduce stress
15 cracking.

PCT Application WO 96/02616 describes the use of lubricant concentrates comprising organic alkyl phosphate esters, aromatic biocidal quaternary ammonium compounds, and sufficient base to provide the concentrate with a pH of from 5 to
20 10.

U.S. Patent No. 4,521,321 describes lubricants for conveyor systems which comprise dilute aqueous systems of partially neutralized monophosphate aliphatic (e.g., saturated or partially unsaturated linear alkyl). The use of a synergist such as
25 long chain fatty alcohol, fatty acid derived amine oxide, or urea improves the properties of the lubricant.

U. S. Patent No. 5,062,979 describes lubricants for conveyor systems

comprising aqueous, clear solution-forming, substantially soap-free compositions. These lubricants comprise pH 6-8 compositions comprising alkyl benzene sulfonates, partial phosphate esters with alkoxyated aliphatic alcohols, and aliphatic carboxylic acids. Typical additives such as solubilizers, solvents, foam inhibitors
5 and disinfectants may also be present. The aliphatic carboxylic acids are C6-C12 fatty acids.

SUMMARY OF THE INVENTION

Lubricating compositions of the invention, especially those designed for use
10 in beverage conveying systems for contained beverages, comprise at least the following components:

- a) an alkyl alkoxyated (e.g., ethoxyated or propoxyated, preferably ethoxyated) phosphate ester,
- b) aryl (e.g., aromatic, such as phenol) alkoxyated (e.g., ethoxyated or
15 propoxyated) phosphate ester,
- c) an aromatic or linear quaternary ammonium antimicrobial agent, and
- d) a liquid carrier, such as water.

Particularly desirable optional agents with high degrees of utility include chelating
20 agents (e.g., the aminoacetic acid chelating agents such as ethylene diamine tetraacetic acid, EDTA), detergents (e.g., nonionic surfactants) and pH control agents, e.g, potassium or sodium hydroxide.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows a graph of data relating the Coefficient of Friction (kinetic) for phosphate esters alone, versus phosphate esters mixed with quaternary ammonium biocides.

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Figure 2 shows a graph of data relating the Coefficient of Friction (kinetic) of phosphate esters lubricating compositions containing either linear quaternary ammonium biocides or aromatic quaternary ammonium biocides.

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Figure 3 shows a graph of data relating the Coefficient of Friction (kinetic) for a lubricant composition of the invention as compared to various lubricant compositions with various couplers (e.g., hydrotropes).

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Figure 4 shows a triangular graph of the effects of variations among anionic surfactants, cationic surfactants and beverage in the practice of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

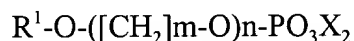
Lubricant compositions according the present invention comprise at least the following components:

- a) an alkyl alkoxyated (e.g., ethoxylated or propoxylated, preferably ethoxylated) phosphate ester,
- b) phenol alkoxyated (e.g., ethoxylated or propoxylated) phosphate ester,
- c) an aromatic or linear quaternary ammonium antimicrobial agent, and
- 25 d) a liquid carrier, such as water.

The lubricating compositions are usually provided as concentrates which are diluted with the appropriate liquid (e.g., usually water) to up to a 400 times dilution to provide a use solution of the lubricant composition. These compositions are capable

of providing a number of beneficial properties as lubricant use solutions, and especially as lubricant use solutions for conveying systems for beverage containers. Each of the ingredients and the various types of properties sought for the lubricant compositions are described below. "Lubricant compositions" is a term used to cover both the lubricant concentrate and the lubricant use solution which is formed by dilution of the concentrate with the appropriate thinning liquid, usually water.

An alkyl alkoxyated (e.g., ethoxylated or propoxylated, preferably ethoxylated) phosphate ester has the general structural formula of:



wherein R^1 comprises an alkyl group (e.g., linear, branched or cyclic alkyl group of from 1 to 20 carbon atoms, preferably of from 8 to 12 carbon atoms),

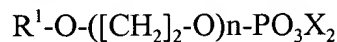
m is 2 or 3,

n is 3 to 8 when m is 3, and 3 to 10 when m is 2, and

X is hydrogen, an alkanolamine and/or an alkali metal.

The alkyl groups of R^1 may be variously substituted so as to provide a variety of subtle changes in its physical properties, especially with respect to its solubility (e.g., the addition of solubilizing groups or pH adjusting groups) and ionic qualities.

Where the phosphate ester comprises an ethoxylated phosphate ester structure, another representative formula would be:



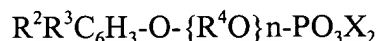
wherein R^1 comprises an alkyl group (e.g., linear, branched or cyclic alkyl group of from 1 to 20 carbon atoms, preferably of from 8 to 12 or 10 to 12 carbon atoms),

n is 3 to 8 or 3 to 10, preferably from 4 to 6 with a weight average of about 5, and

X is hydrogen, an alkanolamine and/or an alkali metal.

An aromatic (e.g., aryl, phenol, naphthol, etc.) alkoxyated (e.g., ethoxylated

or propoxylated) phosphate ester has the general formula of:



wherein R^2 and R^3 may be independently selected from the group consisting of hydrogen and alkyl group (e.g., linear, branched or cyclic alkyl group of from 1 to 20 carbon atoms, preferably of from 8 to 12 carbon atoms),

R^4 is selected from $-CH_2CH_2-$ and $-CH_2CH_2CH_2-$ (ethylene and propylene), and

n and X are as defined above.

Again, alkyl groups of R^2 and R^3 may be variously substituted so as to provide a variety of subtle changes in its physical properties, especially with respect to its solubility (e.g., the addition of solubilizing groups or pH adjusting groups) and ionic qualities. At the present time, it is preferred that R^2 and R^3 are hydrogen.

The aromatic and/or linear quaternary ammonium antimicrobial agents are materials generally known in the antimicrobial art. This class of compounds may be generally represented by the formula:



wherein R^5 , R^6 , R^7 and R^8 are selected from the group consisting of aryl (e.g., phenyl, furyl, etc.), alkyl arene (e.g., benzyl), and alkyl group. When any one or more of R^5 , R^6 , R^7 and R^8 are aryl or alkyl arene, the compound is referred to in the art as an aromatic quaternary ammonium compound. It is preferred that no more than two of R^5 , R^6 , R^7 and R^8 have more than 4 carbon atoms, with 8 to 18 carbon atoms being preferred for longer chain alkyl groups. It is possible to have all four of R^5 , R^6 , R^7 and R^8 have from 1 to 4 carbons atoms, with 8-18 carbon atoms preferred, and with independent variations in the number of carbon atoms in the groups and distribution of these groups within the compounds being acceptable.

It is preferred that the composition contain a basic compound, e.g., an alkali

metal hydroxide or ammonium salt to control the pH. It is preferred that the composition has a pH of less than 8.5, more preferred that it have a pH less than 8.0 and more preferably that it have a pH between 4.5 and 8.0 or 6.0 and 8.0. The control of the pH level within the range of about 6.0 to about 8.5 has been found to provide another unique benefit to the compositions of the present invention. The microbial activity of the compositions tends to increase significantly when the compositions of pH 6.0 to 8.5 have their pH levels reduced, as by contact with acidic beverages (which most commercial beverages and juices are). This increased activity upon exposure to beverages with a pH lower than that of the lubricant preserves the antimicrobial activity until such time as the activity is needed most, when sustenance is provided for the growth of the microbes, e.g., by the spillage of beverages. As the presence of the beverage tends to reduce the pH of the lubricant, the activity of the antimicrobial agent is better preserved and more efficiently used by such activation.

Although the lubricant compositions of the present invention are novel with any combination of

- a) an alkyl alkoxyated (e.g., ethoxylated or propoxylated, preferably ethoxylated) phosphate ester,
- b) aromatic (e.g., phenol) alkoxyated (e.g., ethoxylated or propoxylated) phosphate ester,
- c) an aromatic or linear quaternary ammonium antimicrobial agent,

(with or without a liquid carrier) there are ranges and proportions of these combinations which provide improved or enhanced performance as compared to the broad range of compositions. For example, the relative proportion of anionic to cationic materials in the lubricant composition (i.e., the relative proportions of the combined total of phosphate ester [anionics] compared to the total of quaternary ammonium microbial agents on a weight to weight basis) affects the degree to

which sedimentation, precipitation, cloudiness and deposits occur in the lubricant compositions when contacted with beverages. The higher the proportion of anionics to cationics, the more strongly the compositions resist deposits. It is preferred that the proportion of anionics to cationics is at least 1.5, usually within the range of 2.0 to 10.0, more preferably within the range of 2.0 to 8.0. As noted, the greater the amount of beverage to which the lubricant is likely to be exposed, the higher the preferred ratio of anionics to cationics. The proportions of materials within the concentrate compositions may also be described in terms of 7-30 weight percent anionic materials and 1-5 weight percent cationic materials. These percentages allow for a maximum range of about 30:1 to 1.28:1 ratios by weight of anionic materials to cationic materials. Unless otherwise stated, all proportion described in the examples are percentages by weight. Figure 4 shows some of these interactive effects.

Additional ingredients which do not significantly and adversely affect the stability and lubricating properties of the composition may also be present in the compositions of the invention. Coupling agents, that is materials which have an affinity for both hydrophilic and hydrophobic materials may be included within the compositions. Coupling agents are also referred to as hydrotropes, chemicals which have the property of increasing the aqueous solubility of variously slightly soluble organic compounds. The compounds often have both hydrophilic and hydrophobic functionalities within a single molecule to display affinity to both environments, and are commonly used in the formulation of liquid detergents.

Another attribute of the present invention is that the lubricants of the invention tend to have a wider range of utility with respect to the container material and the conveyor material. It has usually been the practice in the art to specifically design lubricant compositions for use with particular container compositions and

conveyor support materials. The supporting surfaces on conveyors may comprise fabric, metal, plastic, composite and mixtures of these materials. Lubricants would preferably be compatible with a variety of these surfaces. Similarly, bottle compositions may comprise metals, glasses, papers, treated papers, coated papers, laminates, ceramics, polymers, and composites, and the lubricant compositions would preferably have a range of compatibility with all of these materials. Although there may be some variation in the quality of performance with certain materials, the lubricants of the present invention do tend to display a greater latitude in acceptable performance with a range of materials than many lubricant compositions.

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Possible optional agents with high degrees of utility include chelating agents (e.g., EDTA), nonionic detergents, and alkalating agents, e.g., potassium, sodium hydroxide, or alkanolamines. The preferred chelating agents for use in the practice of the present invention are the amine-type acetic acids. These chelating agents typically include all of the poly(amine-type) chelating agents as described in U.S. patent No. 4,873,183. Other chelating agents such as nitrilotriacetic acid, alkali metal salts of glucoheptanoate, and organic substituted phosphoric acid, and their equivalents are also useful in the practice of the present invention. The chelating agents are preferably present as from 0.05 to 10% by weight of the lubricant concentrate composition, preferably from 0.05 to 2% by weight.

20

In a synthetic lubricant environment, the invention has found that quaternary ammonium antimicrobial agents, and especially the linear quaternary compounds act as lubricants in combination with the linear and phenol phosphate esters. At least one of the referenced art (e.g., PCT GB95/01641, page 17, lines 12-18) specifically shows that the combination of quaternary ammonium compounds with the alkyl (linear) phosphate esters did not affect lubricity. The finding that the combination of the quaternary ammonium antimicrobial agents with the combination of esters of

the present invention actually increases lubricity (reduces the coefficient of friction) provides a basis for the assertion of unexpected results in the defined chemical classes of compounds.

5	Exemplary Formula		
	Raw Material	Chemical Name	(%)
	Soft water		65.50
10	Phosphate Ester	C ₁₀₋₁₂ alkyl phosphate ester, 5 EO units	12.50
	Rhodafac TM	phenol ethoxylated phosphate ester	2.50
	RP-710		
15	Bardac TM 2250	didecyl dimethyl ammonium chloride, 50%	5.00
	Versene TM 100	EDTA, 40%	10.00
20	NaOH, 50%	NaOH	2.00
	Neodol TM 25-7	C ₁₂₋₁₅ linear alcohol, 7 EO	2.50
			100.00

25 **EXAMPLE 1**

Two formulae were prepared as set out below. The first formula contained the blended phosphate esters, EDTA, NaOH, and linear quaternary ammonium antimicrobial agent. The second formula was identical with the exception of the linear quat.

30 0.1% use solutions of each formula were prepared in softened water. This solution was sprayed on the short track conveyor which was set up with glass bottles held stationary as the stainless steel conveyor rotated at 100 rpm. The drag was measured with a load cell, which was in turn connected to a computer which plotted the COF (kinetic) based on the drag and the load. The results are presented below in

35 Figure 1, a graph displaying the coefficient of friction (COF) versus time for a phosphate ester with a linear quat versus a phosphate ester used alone.

Formulas

	Raw Material	Chemical Name	Formula (%)	
			10-1	10-2
5	Soft Water		68.0	73.0
	PE	C ₁₀₋₁₂ alkyl phosphate ester, 5 EO units	12.5	12.5
	PR-710	phenol ethoxylated phosphate ester	2.5	2.5
10	Versene™ 100	EDTA, 40%	10.0	10.0
	NaOH	NaOH	2.0	2.0
15	Bardac™ 2250	didecyl dimethyl ammonium chloride, 50%	5.0	0.0
			100.0	100.0

Conclusions

- 20 The inclusion of linear quat in the formula improves the lubricity over a lubricant containing only the blend of phosphate esters.

EXAMPLE 2

- 25 Two formulas of lubricating agents were prepared as set out below. The first formula contained the blended phosphate esters, EDTA, NaOH, nonionic surfactant, and linear quaternary ammonium antimicrobial agent. In the second formula, the linear quaternary ammonium antimicrobial agent was replaced with benzyl quat.

- 30 0.1% use solutions of each formula were prepared in softened water. This solution was sprayed on the short track conveyor which was set up with glass bottles held stationary as the stainless steel conveyor rotated at 100 rpm. The drag was measured with a load cell, which was in turn connected to a computer which plotted the COF (kinetic) based on the drag and the load. The results are presented in Figure 2 which shows a comparison of COF versus time for phosphate esters with either a

linear quat or a benzyl quat.

Formula

5	Raw Material	Chemical Name	Formula	
			(%)	
			KX	10-3
	Soft Water		68.0	68.0
10	PE	C ₁₀₋₁₂ alkyl phosphate ester, 5 EO units	12.5	12.5
	PR-710	Phenol ethoxylated phosphate ester	2.5	2.5
	Versene™ 100	EDTA, 40%	10.0	10.0
15	NaOH	NaOH	2.0	2.0
	Bardac™ 2250	didecyl dimethyl ammonium chloride, 50%	5.0	0.0
20	Q-372	benzyl quat, 50% (a mixture of alkyldimethyl- benzyl ammonium chlorides)	0.0	5.0
			100.0	100.0

Conclusions

- 25 The linear quat species improves the lubricity of the formula as compared to the benzyl quat.

EXAMPLE 3

- 30 Two formulae were prepared as set out below. The first formula contained blended alkyl and aryl phosphate esters and the second formula contained only alkyl phosphate ester. Both formulas contained EDTA, nonionic, NaOH, and linear quat.

The viscosity of the concentrates was measured in triplicate on a Brookfield viscometer model RVT at 51, 78 and 116°F (spindle #3, 100 rpm, factor = 10).

The results are provided below.

5 Formula

	Raw Material	Chemical Name	Formula (%)	
	Soft Water		65.50	65.50
10	PE	C ₁₀₋₁₂ alkyl phosphate ester, 5 EO units	15.00	12.50
	Versene™ 100	EDTA, 40%	10.00	10.00
15	NaOH, 50%	NaOH	2.00	2.00
	Bardac™ 2250	didecyl dimethyl ammonium chloride, 50%	5.00	5.00
	Neodol™ 25-7	C ₁₂₋₁₅ linear alcohol, 7 EO	2.50	2.50
20	Rhodafac™	phenol ethoxylated		2.50
	RP-710	phosphate ester		
			100.00	100.00
25				

Results

	Temperature (°F)	Phosphate Ester(s)	Average Viscosity (cps)
5	51	Alkyl and Phenol blend	50
	78	Alkyl and Phenol blend	51
10	116	Alkyl and Phenol blend	49
	51	Alkyl	170
15	78	Alkyl	132
	116	Alkyl	64

Conclusions

Blending phenol phosphate ester with alkyl phosphate ester in the formula reduces the viscosity at all temperatures tested and the resultant low viscosity appears to be temperature independent. This property provides for ease of application on a conventional conveyor apparatus.

EXAMPLE 4

Formulas containing alkyl phosphate ester and linear quat were prepared with various nonionic and anionic adjuvants to determine the affect on lubricity. A control containing phenol phosphate ester, a control with higher level of alkyl phosphate ester, and a control with no adjuvant were prepared for comparative purposes. The formulas are provided below.

0.1% use solutions of each formula were prepared in softened water. This solution was sprayed on the short track conveyor which was set up with glass bottles held stationary as the stainless steel conveyor rotated at 100 rpm. The drag was measured with a load cell, which was in turn connected to a computer which plotted the COF based on the drag and the load. Each sample was run two or more times, and the average COF was calculated. The results are provided in Table A below.

Formulas

Table A

Raw Material	Chemical Name	1	2	3	4	5	6	7
Soft Water	above	68.00	65.50	61.70	65.50	65.50	65.50	65.50
PE-362	above	12.50	15.00	12.50	12.50	12.50	12.50	12.50
Versene™ 100	above	10.00	10.00	10.00	10.00	10.00	10.00	10.00
NaOH, 50%	above	2.00	2.00	2.00	2.00	2.00	2.00	2.00
Bardac™ 2250	above	5.00	5.00	5.00	5.00	5.00	5.00	5.00
Neodol™ 25-7	above	2.50	2.50	2.50	2.50	2.50	2.50	2.50
SXS, 40%	Na/xylene Sulfonate			6.30				
Rhodafac™ RP-710	above				2.50			
Polysorbate™ 80	sorbitan monooleate					2.50		
Glucopan™ 625CSUP	Alkyl poly glycoside						2.50	
Triton™ X-102	octyl phenol ethoxylate							2.50

Conclusions

The phenol and alkyl phosphate esters improved lubricity over the control, while none of the other adjuvants showed this advantage.

5 EXAMPLE 5

This example examines the ratios of phosphate ester and quat which do not interact with beverage to form a precipitate. A 40% phosphate ester solution in soft water was combined with 10% active linear quat solution in water and a cola beverage at various levels. After one day, the samples were observed for clarity.

- 10 Samples were rated as clear, hazy, and separated. (Over time, all hazy samples formed precipitates.)

Results

See the ternary plot in Figure 4.

15

Conclusions

At higher levels of beverage a higher ratio of anionic to cationic surfactant is required to maintain clarity. The ratio ranges from about 1.5:1 at very low levels of beverage, to 2.5:1 at 50% beverage and 16:1 at very high levels of beverage.

20